The 1994 Sefidabeh (eastern Iran) earthquakes revisited: new evidence from satellite radar interferometry and carbonate dating about the growth of an active fold above a blind thrust fault

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SUMMARY

In 1994, three shallow earthquakes of $M_w \sim 6$ occurred close together on blind thrusts near Sefidabeh in eastern Iran. In an earlier study of the teleseismic waveforms, the geomorphology and the faulting in the epicentral region, it was suggested that these earthquakes were associated with the growth of a ridge above a blind thrust fault system, whose activity could be detected by its effect on the surface drainage. In this study we present a SAR interferogram that precisely determines the location and amount of coseismic surface displacements, showing that the earthquakes in the Sefidabeh sequence probably occurred on en-echelon fault segments associated with three stepping ridges. We also present U/Th dates of ~ 100 ka for lake deposits uplifted by the growing ridge. From the cumulative, dated uplift and knowledge of the surface displacements due to an earthquake sequence, we estimate that ~ 120 such events have occurred in the past 100 ka, with an average recurrence interval of 830 yr, and an average convergence rate of 1.5 mm yr⁻¹ on the Sefidabeh thrust; each estimate has an uncertainty of a factor of two, either way. We argue that the Sefidabeh fault originally formed by coalescence of many small fault segments, and has grown in length at about 2 cm yr⁻¹ in the past 100 ka. Though the coseismic surface deformation observed in the SAR interferogram closely resembles folding, the overall topography does not, because of inherited topography associated with earlier geological deformation. In spite of this, the activity of the buried thrust fault can easily be detected by its effect on the surface drainage: a significant lesson when interpreting landscapes that are not entirely due to the present-day deformation.

Key words: continental deformation, earthquakes, geochronology, Iran, SAR interferometry.

1 INTRODUCTION

The topography of tectonically active areas reflects the tectonic processes at work. In particular, the topography associated with active faults must ultimately be due to the cumulative effect of the uplift and subsidence occurring in individual earthquakes. However, if the only information available is the present-day topography itself, then the connection between earthquake deformation and present topography can be made only by assuming the likely deformation due to a single earthquake. Without independent information about the age of the topographic features, nothing can be said about the rates of processes that have created the present landscape. In this paper, we show how additional information from geodesy and modern dating methods can remove many of these uncertainties, by taking a new look at a sequence of four earthquakes, with magnitudes (M_W) 5.5–6.2, that occurred within a few days of each other in 1994 February near the village of Sefidabeh in eastern Iran. The initial study by Berberian *et al.* (2000) of these earthquakes was based on field observations, satellite imagery and seismology, and suggested that the fault system responsible involved blind faulting beneath a NW–SE trending ridge southwest of, and adjacent to the village of Sefidabeh itself (Figs 1–4). Since that study, new information has come from two main sources. First, we have been able to obtain a synthetic aperture radar (SAR) interferogram,







Figure 4. (a) Landsat-7 ETM imagery for the area of Sefidabeh. The image is a false colour composite using band 7 (red), band 4 (green) and band 1 (blue) from a mosaic of ETM images recorded on 2001/06/25 (158/38) and 2001/05/8 (158/39). The uplifted lake deposits are marked with L. (b) Shaded relief for the same area from the InSAR DEM derived in this study. The illumination is from an azimuth of 148° E, that is, parallel to the local ridges, and an elevation of 40° . The banks of the deflected Butgow river (dashed white line) may be seen cutting across the pre-existing river that used to drain directly downslope and later supplied the now-uplifted lake.

enable structural rotations about a vertical axis (Bayasgalan *et al.* 1999; Berberian *et al.* 2000).

2.2 Topography and drainage

In exploring the topography and drainage of the Sefidabeh area, we have made use of a 40-m-resolution digital elevation model (DEM; Fig. 2), the construction of which is described below in the section on InSAR analysis. The Sefidabeh ridge, which rises just over 100 m above the plain beneath it, is superimposed on a regional slope of about 600 m in 30 km (Fig. 3).

Features in the drainage around the Sefidabeh ridge may be highlighted in shaded relief maps with the appropriate direction of illumination (Fig. 4b). In particular, a substantial river, the Rud-e-Butgow, appears to be deflected round the northern end of the ridge. Berberian *et al.* (2000) suggested that prior to the growth of the NW–SE ridge the drainage was directly down the regional slope. As the ridge grew in repeated earthquakes across the path of the river, defeating the river in its attempt to cut through the ridge, a lake formed. Subsequently the river was deflected and the lake drained, leaving the light-coloured deposits that can be seen in the Landsat-7 ETM image in Fig. 4(a). It is these deposits, which are now found \sim 70 m above the Sefidabeh plain, that we sampled and subjected to U-series dating, in order to constrain the age at which the lake deposits ceased to form, and began to be uplifted.

2.3 Earthquake locations

The published teleseismic epicentres of the five main earthquakes in the 1994 Sefidabeh sequence are very close together (Fig. 5; Berberian *et al.* 2000). In an attempt to see whether we could resolve any difference in position between them, we carried out multiple event relocation on the sequence using the hypocentroidal decomposition (HDC) method (Jordan & Sverdrup 1981). The basic method has been updated with modern earthquake location algorithms and data set from the EHB single event algorithm



Table 2. ERS SAR data used in the InSAR analysis.

	Date 1	Orbit 1 ^a	Date 2	Orbit 2 ^a	$B_{\perp}{}^{\mathrm{b}}$	$h_a{}^c$
(1) DEM generation	1996/05/04	25115 (ERS-1)	1996/05/05	5442 (ERS-2)	104	87
(2) Coseismic pair	1993/01/07	7737 (ERS-1)	1996/03/31	4941 (ERS-2)	29	353

^aTrack 77, frame 2985; ERS SAR data © European Space Agency.

 ${}^{b}B_{\perp}$ is the perpendicular baseline, that is, the component of the orbital separation perpendicular to the line of sight from satellite to the ground.

 $^{c}h_{a}$ is the altitude of ambiguity.

in an interferogram—is 87 m. We constructed a SAR interferogram with the tandem pair, and transformed that to a ground registered DEM with a posting of 40 m, using the JPL/Caltech ROI_pac software (Rosen *et al.* 2004). In calibrating the orbital baseline between satellite passes, and in removing residual biases and tilts, the 1 km posting GTOPO30 DEM was used.

Recently a Shuttle Radar Topographic Mission (SRTM) DEM (Farr & Kobrich 2000) was released for this area. The 40-m InSAR DEM and 90-m SRTM DEM agree quite well, apart from a small translation error. The two were matched, and the SRTM topography used to fill in holes in the InSAR DEM. Topography from the resulting DEM is shown above in Fig. 2; quite subtle and coherent features may be observed in shaded-relief maps made from it (e.g. Fig. 4b, Fig. 6). Note, in particular, that the NW–SE ridge next to Sefidabeh is the northern one of a series of en-echelon, right-stepping ridges extending over a distance of about 30 km. Given the arid nature of the area, path differences and hence topographic errors due to tropospheric water vapour are likely to be small. Differences between the InSAR DEM constructed here and SRTM heights have a standard deviation of about 7 m, about the error expected for SRTM alone, suggesting that the errors in the InSAR DEM are probably smaller than those in the SRTM data.

The coseismic interferogram (Fig. 6) was also constructed using the JPL/Caltech ROI_pac software. The topographic corrections were made with the 40-m InSAR DEM; with an altitude of ambiguity of 353 m, range errors due any topographic errors will be \sim 1 mm. The time interval between ERS SAR acquisitions before and after the Sefidabeh earthquakes is slightly longer than 3 years (Table 2). Nonetheless, for the most part the coherence is very high, probably the result of the arid environment and the consequently low rates of surface alteration. The main area of low coherence—the gap on the eastern side of the dominant set of fringes in Fig. 6—is over the Sefidabeh ridge and the en-echelon ridges to the south. A likely reason for this is the bedding-plane slip on near vertical beds



Figure 6. Coseismic interferogram for the epicentral area of the 1994 Sefidabeh earthquakes. This overlies topography as shaded relief derived from the infilled InSAR DEM, which can be seen directly in areas of poor coherence masked in the interferogram. Each colour cycle from blue to red represents an increase of 28 mm in the range to the satellite. The line gives the location of the profile of unwrapped phase shown in the next figure. This figure and those for the model calculations use a Universal Transverse Mercator projection, zone 41.



Figure 7. Phase variations and range changes along the profile shown in Fig. 6. A phase change of 2π is equivalent to a line-of-sight range change of 28.3 mm. We have chosen a sign convention chosen here so that movement towards the satellite (range decrease) corresponds to positive phase.

observed by Berberian *et al.* (2000), which results locally in large displacement gradients and a disturbed surface.

The interferogram is mainly smoothly varying on a length scale of about 15 km perpendicular to the ridges (Fig. 6). It shows the asymmetry typical of a steeply dipping thrust fault between larger hanging wall uplift in the west and smaller footwall subsidence to the east, an asymmetry in the opposite sense to that observed in normal fault earthquakes (e.g. Wright et al. 1999). In the area of subsidence closest to the topographic ridges, the fringes show an en-echelon effect, suggesting separate contributions from slip associated with each of the ridges. A profile of unwrapped phase across the interferogram gives a maximum phase change of about 125 radians, equivalent to about 0.55 m of displacement towards the spacecraft (Fig. 7). If we assume that most of the motion is vertical at the maximum, this corresponds to 0.6 m of uplift. It should be noted that the surface displacements revealed by the coseismic interferogram represent the net deformation of all the events making up the sequence of earthquakes at Sefidabeh. Nonetheless, this magnitude of uplift is of the order expected for earthquakes with $M_w \sim 6.0$, with about 1 m of slip in each event (Berberian et al. 2000). Note also that the wavelength of the uplift, $\sim 10-15$ km, is that expected for reverse faulting in a seismogenic layer 10-15 km thick.

3.2 Modelling of fault plane slip

The interferogram we have derived has phase changes or equivalent line-of-sight surface displacements on an 80 m grid, producing too many values to be easily assimilated in a rapid inversion scheme. In order to reduce the number of data values to be used, we subsample the interferogram using the quadtree method (e.g. Jónsson *et al.* 2002). The mean value of the phase in a block, assumed located at its centre, is used in the modelling if the variance of phase values in the block is less than the noise variance estimated from part of the interferogram away from the coseismic fringes. Otherwise, the block is subdivided into four equal parts and the test repeated. A maximum block size of 7 km was chosen, equal to the length scale of the covariance function of the phase (see Appendix A), again calculated using part of the interferogram away from the coseismic fringes. The number of phase samples was reduced in this way to 1512 from $\sim 3 \times 10^6$ in the full interferogram.

3.2.1 Slip on a single fault plane

An initial attempt was made to model the net displacements produced by the Sefidabeh earthquakes as those due to uniform slip on a single rectangular fault plane, following the approach of Wright *et al.* (1999). The surface displacement vector (**u**) at each point produced by the elastic dislocation was calculated using the expressions given by Okada (1985), and then projected into the satellite line of sight ($\Delta l = -\hat{\mathbf{n}} \cdot \mathbf{u}$), using the unit vector ($\hat{\mathbf{n}}$) pointing to the satellite calculated locally at each observation location. A non-linear, downhill simplex algorithm, with Monte Carlo restarts to avoid local mimina, was used to determine nine fault parameters (Table 3) plus a line-of-sight offset. Formal errors on the fault parameters were obtained as described in Appendix A.

The best-fitting solution with uniform slip on a single fault (column 1, Table 3) fails to predict a number of features, for example, the tapering of the fringes at the south and the angular fringes at the north (Fig. 8a), and consequently there are a number of significant residuals (Fig. 8b). The strike of the fault (161°) is greater than that of each of the en-echelon ridges (148°), but rather represents the average strike of the system of ridges. This suggests that slip may have occurred separately on separate faults related to the ridges, and the uniform single fault model compensates for this by rotating its strike.

To investigate this further, we sought another solution with uniform slip on a single fault where the strike was fixed at that of the ridges (column 2, Table 3). We then extended the length of this fault to 25 km, and from the surface to a depth of 20 km, and solved for distributed slip on this plane with its geometry fixed to that of the

Table 3. Fault parameters for single fault, uniform slip calculations. Eastings and northings are in UTM zone 41, and represent the centre of the line where the fault plane would intersect the surface if extended. Errors (see Appendix A2) are 1 standard deviation rounded to last decimal place. Because of the constrained nature of the three-fault solution, error estimates were not made in this case.

	One	e fault	Three faults		
	Free strike	Fixed strike	1	2	3
Strike	161 ± 1	148	148	148	148
Dip	47 ± 1	46 ± 1	45	45	45
Rake	89 ± 3	68 ± 2	105	105	105
Slip (m)	1.95 ± 0.07	1.78 ± 0.05	1.5	1.5	0.75
Length (km)	12.7 ± 0.1	12.0 ± 0.1	5	7.5	8
Min depth (km)	4.4 ± 0.1	4.0 ± 0.1	5	2.8	4.4
Max depth (km)	10.1 ± 0.2	10.2 ± 0.2	11.7	9.5	9.7
Easting (km)	269.6 ± 0.1	268.2 ± 0.1	269.2	268.3	270.6
Northing (km)	3420.0 ± 0.2	3422.3 ± 0.1	3426.5	3419.8	3412.6
$M_0 \times 10^{18} \text{ Nm}$	6.6 ± 0.1	6.4 ± 0.1	2.4	3.6	1.5
				Total = 7.5	
M_w	6.5	6.5	6.2	6.3	6.1



Figure 8. Model interferograms and residuals for calculations with slip on a single fault. Each colour cycle represents 28 mm of range change. The red lines show where the fault plane, if extended, would intersect the surface. (a) Model interferogram with uniform slip on fault (see Table 3). (b) Residual (observed minus model) fringes for uniform slip calculation. (c) Model interferogram with distributed slip on extended fault plane. (d) Residual fringes for the distributed slip calculation.

fixed-strike, uniform-slip solution. The method used to obtain the distribution of slip is described in Wright *et al.* (2004). The fault surface was divided into 80 patches, each 2.5 km long and 2.5 km high, the line-of-sight surface displacements due to slip on each patch being calculated using the expressions of Okada (1985) as before. To prevent unphysical oscillatory slip or retrograde motion on the fault, Laplacian smoothing was imposed. There is a trade-off between the roughness and the rms misfit of the solution; the weighting of the Laplacian smoothing was chosen to give a solution that had both low misfit and roughness (Wright *et al.* 2004). Errors for this non-linear inversion were determined using the method described in Appendix A.

The resulting slip distribution is given in Fig. 9, with the predicted line-of-sight displacements and the corresponding residuals shown in Figs 8(c) and (d). The interferogram does a better job at predicting the shape of the fringes in the north, but there are still some significant residuals at the southern end of the faulting, where the model interferograms seem too rounded.

3.2.2 Slip on three fault planes

The surface displacements are actually the combined effect of similar earthquakes located close to each other. The limitations to how well we could reproduce the interferogram with slip on a single fault, and the features of these solutions, suggests that the slip occurred on more than one fault plane, possibly associated with the different ridge segments seen in the topography. We, therefore, decided to try to find a model with slip on three fault planes, as three of the events in the 1994 Sefidabeh sequence are larger than the others (Table 1; Berberian *et al.* 2000).

The lengths of the fault segments were estimated from the ridge segments in the topography, constrained by the location of the ends of the fault in the single fault solution. Guided by the single fault solutions and the seismic source mechanisms of Berberian *et al.* (2000), the strike (148°), dip (45°), rake (105°), and slip (1.5 m) were then all fixed, and we then solved for minimum and maximum depth of faulting and location of each segment. This solution was further refined by fixing everything apart from the slip and depth extents on the southern segment (Table 3). Given the highly constrained nature of this calculation, we did not attempt a formal error analysis.

The total moment we obtain (Table 3) is about 40 per cent larger than the combined seismic moment, perhaps not surprising considering the long time interval spanned by the interferogram. The relative moments we calculated for each of the segments are very



Figure 9. (a) Slip and (b) associated errors for distributed slip on a single fault. The model interferogram and residual fringes calculated with this slip distribution are shown in Figs 8(c) and (d).

similar to those determined seismologically for the separate events (Table 1; Berberian *et al.* 2000), and the centres of the individual fault segments are similar in depth to the centroids determined seismologically, which are all in the range 5–10 km (\pm 4 km). The predicted and residual solutions for this source model are shown in Fig. 10. The shape of the southern part of the interferogram is improved, but the angular northern feature is not well represented. There are still significant residuals, largely at the offsets between segments.

We then extended the length of the northern segment to the north, and the length of the southern segment to the south, and extended all segments in depth. A variable distribution of slip was then sought on each fault segment as before, the faults being divided into a total of 144 patches, with dimensions of 2.5 km in length and 2.5 km in depth as before (Fig. 11). The interferogram is now reasonably well reproduced, the residuals generally being small and randomly distributed (Figs 10c and d).

The modelling is obviously highly non-unique. Nonetheless, we feel it is a reasonable hypothesis, based on the above calculations, that the earthquakes in the Sefidabeh sequence occurred on separate fault segments. As discussed in Section 2.3, although we know the relative locations of the Sefidabeh earthquakes events well, the absolute location of the cluster is subject to bias. The centre of the cluster lies about 10.4 km away on an azimuth of 170° from the centre of the area of significant fault slip. If we remove this bias by shifting the cluster by 10.4 km in the opposite direction, we can see that the extent of the area of maximum slip in Fig. 11 compares well with the spread of earthquake locations. We also note that the regions of maximum slip on the fault segments in Fig. 11 appear to be aligned, suggesting that slip on one segment may then have triggered slip on its neighbour.

4 PETROGRAPHIC AND ISOTOPE ANALYSIS OF THE SEFIDABEH CARBONATES

The carbonates that are preserved in the now-abandoned and uplifted gorge near the village of Sefidabeh potentially contain information about the chronological and climatic history of the uplifted ridge and its drainage system. Understanding the climatic history is important, if we are to exploit signals in the landscape related to the evolution of drainage patterns for tectonic purposes. We took six samples from a prominent bluff exposed at the top of the carbonate section, overlooking Sefidabeh (Fig. 12). Details of the petrography and isotope analysis are given in Appendix B. Only a summary of the pertinent results are given here in the main text.

The deposit, wrongly identified as a travertine by Berberian et al. (2000), is essentially a calcite-cemented sandstone, which in its upper part has been almost totally cemented or replaced by nonferroan early diagenetic calcite. These calcites contain petrographic evidence of microbial activity and at least three cement stages including some dripstone fabrics indicative of vadose zone conditions (i.e. above the water table) at times. Numerous vugs or fenestrae are common and these are now partially cemented. Some of the vugs may have contained evaporite salts, now dissolved. The environment of deposition seems to have been a sandy fluvial system draining a playa lake. Calcite formation either happened when surface drainage waters dried out, or more likely occurred in and around groundwaterfed springs, where carbonate formation is encouraged by degassing of dissolved CO2. Upward-flowing groundwater caused rupturing of cemented crusts and development of fenestrae. Similar fenestral limestones, but with extensive aragonite cementation in this case, are known from semi-arid carbonate flats in south Australia (Ferguson et al. 1982). Overall, calcite cementation clearly occurred in conditions that were wetter than today, presumably as springfed drainage from the now-abandoned playa. Moreover, the petrographic evidence of well-preserved non-ferroan early diagenetic fabrics imply that the carbonates have been unaffected by later diagenetic alteration and are unlikely to have undergone extensive isotopic exchange.

A high priority was to estimate the depositional age of the carbonates. The uranium–thorium technique is well established as a reliable method for dating a wide variety of Mid-Late Pleistocene secondary carbonates (Schwarcz 1989; Ivanovich & Harmon 1992). It depends on the ingrowth of ²³⁰Th from ²³⁴U decay, a process which takes 400–500 ka to reach equilibrium. Thus the relative activity of ingrown ²³⁰Th gives a direct measurement of sample age. Necessary pre-conditions are that the carbonate should (a) initially contain no ²³⁰Th and (b) remain an isotopically closed system.

However, in common with many subaerial carbonates, the Sefidabeh calcite cement incorporates thorium- and uraniumbearing siliciclastic detrital material in the form of sand, silt and clay, thus violating pre-condition (a) above. Such deposits (often referred to as 'dirty calcites') require more intensive U- and Thisotopic study in order to determine an age. One common approach is to analyse several coeval subsamples, containing varying concentrations of the detrital contaminant, to recover isotopic data, which can then be plotted in U-Th isotope ratio space. Such plots define mixing lines (isochrons) between the pure calcite and pure detritus end members. The slopes or intercepts can be used to calculate sample age, depending on the isotope pairs plotted. This approach has been discussed in detail by Ku & Liang (1984), Schwarcz & Latham



Figure 10. Model interferograms and residuals for calculations with slip on three en-echelon faults. The red lines show where the fault planes, if extended, would intersect the surface. (a) Model interferogram with uniform slip on faults (see Table 3). (b) Residual (observed minus model) fringes for uniform slip calculation. (c) Model interferogram for distributed slip with northern and southern fault planes extended. (d) Residual fringes for the distributed slip calculation.

(1989), Bischoff & Fitzpatrick (1991) and Luo & Ku (1991) and partially reviewed by Kaufman (1993). Ludwig & Titterington (1994) and Ludwig (2003) have discussed the statistical treatment of the sample data. Wide variation in contaminant concentration between subsamples is advantageous because this increases the prospect of obtaining a wide dispersion of isotopic ratios and hence better isochron definition. Commonly, however, detrital distribution within a carbonate deposit is rather homogenous, resulting in a compression of the isotopic data range that, when combined with analytical scatter, weakens isochron linearity. The samples analysed here were collected from a single locality within the tufa and the insoluble detrital content of the samples lay within the rather narrow range of 9–16 per cent.

The dating results are detailed in Appendix B2. Plotting 230 Th/ 232 Th versus 234 U/ 232 Th, five of the six data points lie within one standard deviation of the best-fit isochron, whilst one falls almost two standard deviations below the line. This contrasts with the 234 U/ 232 Th versus 238 U/ 232 Th isochron, where all six points lie very close to the fitted line. There is no incontrovertible *a priori* reason for rejecting this outlying point (although see Appendix B2) but, be-

cause it is highly influential, in constructing a six-point isochron we have used a robust, non-parametric regression algorithm of Ludwig (2001). This makes no assumptions about the causes of the observed data scatter and reduces the weighting given to such outliers. Based on the slope of the isochrons, the age of the Sefidabeh deposit is calculated to be 103^{+164}_{-57} ka (Table B2). Omitting the outlying datum, five-point isochrons yield an age of 99^{+30}_{-24} ka (Figures B1 and B2, Table B2).

These age estimates are sufficiently good to allow us to make quantitative estimates of likely fault growth rates and earthquake recurrence times, which are discussed in Section 5. However, the uncertainty in age has significance for climatic interpretations. The stable oxygen isotopic composition of the Sefidabeh calcite (Appendix B3) is relatively light (the mean value of δ^{18} O is $-5.6\%_0$): too light for normal meteoric waters originating from the Indian Ocean today. Light values can be achieved by two effects: either by precipitation from water that has spent considerable time over continents or high elevation (the 'continent/orographic' effect), or from prolonged very heavy rainfall (the 'amount' effect). At Sefidabeh, the first can be achieved if the rainfall originates from the Mediterranean (which



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Figure 13. Location of topographic profiles across and along the Sefidabeh ridge shown in Figs 14 and 15. The profiles are drawn on a shaded relief map of the area, with illumination from an azimuth of 58° and an elevation of 40° .

factor of two either way. Given the age of ~ 100 ka for the uplifted lake deposits, the average recurrence interval is therefore about 830 yr, again with the same level of uncertainty (420–1660 yr). Again using a peak slip on the faults of $\sim 1.5-2$ m, and a dip of 45°, the convergence rate across the Sefidabeh faults is 1.5 mm yr⁻¹ (0.7–3 mm yr⁻¹). From the known height and measured age, the average uplift rate is 0.7 mm yr⁻¹.

Berberian *et al.* (2000) also considered how the Sefidabeh thrust might have grown in length. They used a result of Cowie & Scholz (1992a) for the number of earthquakes N required to increase the length of a fault from an initial value L_0 to a length L:

$$N = \frac{\log L/L_0}{\log(1 + \alpha/\gamma)}$$

where α is the ratio of mean slip during an earthquake to the fault length, and γ is the ratio of mean accumulated displacement on a fault to its length. The ratio $r = \alpha/\gamma$ represents the proportional increase in fault length during each earthquake. Estimating that $L/L_0 \sim 1.9$, and using a value of $r = \sim 1.5 \times 10^{-3}$, they concluded that about 430 earthquakes were required, rather more than the number of earthquakes required to uplift the lake deposits.

If a fault increases in length by the same proportion of its length in each earthquake throughout its history, and the slip that occurs in each earthquake is proportional to the length, then the cumulative offset on the fault would be expected to vary smoothly along its length from a maximum at its centre (e.g. Cowie & Scholz 1992b). However, if we examine a topographic profile along the length of the Sefidabeh ridge (Fig. 15), a somewhat different picture emerges. The cumulative offset, as measured by the height of the ridge above the plain at its foot, is roughly constant between distances of 2.6 and 8.2 km along the profile, falling off rapidly at its edges. This is suggestive of an alternative picture of fault growth, in which there are initially many small faults that rapidly coalesce to form a single longer fault, such that subsequently the slip in each earthquake and hence the cumulative offset is approximately constant along this initial length (e.g. Cowie 1998). Hence, at the time the lake was abandoned and the river Butgow was deflected by the growing ridge, it may well have already extended about 4 km north of the lake deposits. If we assume that $L_0 = 5.6$ km, that is, the segment of roughly constant height above the plain, and that the river always flows around the northern end of the growing ridge, then a better estimate of L/L_0 is 1.3. From eq. (5), this leads to a new estimate of 175 for the number of earthquakes required, well within the range estimated from the amount of uplift, even without allowing for uncertainties in the value of r. If the ridge has propagated 2 km



Figure 15. Topographic profiles along the crest of the Sefidabeh ridge and parallel to the ridge across the plain at its foot. Locations of the profiles are shown in Fig. 13. The arrow marks the location of the uplifted lake deposits.

in 115–230 earthquakes, then the increase in length per earthquake has been 8.7-17.4 m, with an average propagation rate of 2 cm yr⁻¹.

Apart from quantifying and locating the slip in the 1994 earthquakes, and providing evidence of timing and hence deformation rates, this study has one more significant contribution to make. It confirms the suggestion, implicit in Berberian *et al.* (2000), that we can correctly interpret the evidence in the landscape for active, blind thrust faulting. In the case of Sefidabeh, even though the coseismic deformation resembles folding, the overall topography does not (Figs 3 and 14) because of inherited earlier deformation. Nonetheless, the pattern of deformation due to current activity is unmistakeable, in the form of recent changes in drainage incision and deflection. This is a significant lesson in what to look for in those places where active folds do not necessarily resemble folds in their surface shape and the topography as does happen in simpler places (e.g. Keller *et al.* 1998; Jackson *et al.* 1996).

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APPENDIX A: InSAR ERROR ANALYSIS

To determine parameter errors for our non-linear inversions, we followed the method of Wright *et al.* (in preparation), who use the Monte Carlo simulation of correlated noise. This method accounts for the spatial correlations in the atmospheric and orbital components of InSAR noise. It has three stages:

- (1) analysis of InSAR noise;
- (2) simulation of noisy data sets and

(3) inversion of noisy data sets to determine uncertainties in model parameters.

We first determined a best-fit 1-D covariance function, for example, Hanssen (2001), that approximates the noise in coseismic interferogram by analysing a \sim 50 by 50 km region in the northwest of the image, where no significant coseismic displacements occurred.

mean of zero and a standard deviation of 1, by

where \mathbf{L} is the Cholesky decomposition of the variance-covariance matrix, $\Sigma = \mathbf{L}\mathbf{L}^{T}$, (Rubinstein 1981). The correlated noise is then added back to the original data vector to give a new noisy data set. We repeated this procedure 100 times to provide an ensemble of noisy data sets.

Each of these noisy data sets is then used in the appropriate inversion procedure to give a set of model parameters. The distribution of these model parameter gives their error. One advantage of this method is that it also enables us to determine the trade-offs between different model parameters. An example is given in Fig. A1 for our single fault inversion, where we have plotted every parameter against every other parameter for the 100 different inversion results. Several strong trade-offs are evident, such as between

Figure A1. Model parameter trade-offs for uniform-slip model. Each of the 100 dots in each of the upper plots is the best-fit solution for one data set to whicl Monte Carlo, correlated noise has been added. Histograms summarize the results for each parameter.

slip and the minimum depth of faulting, and between rake and *y*-coordinate.

APPENDIX B: ANALYSIS OF THE SEFIDABEH CARBONATES

B1 Petrographic description

Fabric descriptions are based on hand specimens and stained (Dickson 1965) thin-section information. Cathodoluminescence (CL) analysis of thin sections was done using a cold cathode Technosyn instrument run at accelerating voltage of 18–20 kV and a gun current of 180–200 μ A.

The deposit comprises a basal 3.0 m of fine-medium calcite cemented sandstone passing upward into 2.10 m of progressively better cemented sandy limestone, superficially resembling travertine. The basal sandy unit contains angular breccia fragments and blocks of bedded sandy limestone. Bedding and degree of calcite cementation become progressively more pronounced upward in the upper unit, resulting in 0.70-m-thick cap of tightly cemented limestone at the top of the deposit. The better-cemented limestones taste salty and contain abundant millimetre-sized, irregular vugs that crudely follow bedding. Botryoidal calcite cement lines the walls of many of these vugs.

Thin sections show these limestones to be composed of nonferroan micrites and microspars with variable amounts of sandy detritus. The detritus is mainly composed of quartz and feldspar, although CL shows that 2–5 per cent of the sand grains are reworked basement limestone clasts. Ostracod carapaces are the only fossil remains and these are rare. The micrites contain clotted, wispy and cellular fabrics which are probably of microbial origin. In places peloidal or ped-like micritic fabrics are common, associated with patchy accumulations of microspar. Botryoidal non-ferroan radial calcite cement lines the walls of many of the vugs, and some have dripstone fabrics. Smaller former open spaces are partially or wholly infilled by non-ferroan sparry calcite cement. The vugs were probably formed by upward-flowing groundwater that ruptured cemented crusts (*cf.* Ferguson *et al.* 1982), although some may have contained evaporite salts.

B2 U-series dating

Dating method

We used the leachate (L/L) method of analysing contaminated carbonates (Schwarcz & Latham 1989). Seven samples were dissolved in ²²⁹Th/²³⁶U-spiked dilute HNO₃ (\leq 2 M with the exception of one sample which was leached in 5 M), for a standard time. After filtering and concentration of U and Th on FeOH₃, U and Th were separated and purified on anion exchange columns in the nitric form, electroplated onto stainless steel discs from an ammonium sulphate solution and alpha counted.

Results are shown in Table B1 and plotted in isotope ratio space in Figures B1 and B2. The U-series age equation may be written as:

where λ_0 and λ_4 are the decay constants for ²³⁰Th and ²³⁴U, respectively, and *t* is the age, determined iteratively (Kaufmann & Broecker 1965).

 Table B1.
 U-series isotope ratios for Sefidabeh S7 calcite cement samples.

 Errors shown are 1 standard deviation counting statistics.

Lab No	U (ppm)	$^{234}U/^{232}Th$	$^{238}U/^{232}Th$	²³⁰ Th/ ²³² Th
UEA802	0.47	10.701 ± 0.789	6.383 ± 0.473	11.514 ± 0.660
UEA810 UEA811	0.40	8.237 ± 0.430 12.621 ± 0.749	4.867 ± 0.263 7.345 ± 0.444	11.340 ± 0.308 14.202 ± 0.702
UEA879	0.53	11.404 ± 0.752	6.485 ± 0.447	13.565 ± 0.681
UEA880	0.58	10.716 ± 0.699	6.278 ± 0.418	12.430 ± 0.697
UEA881	0.39	9.214 ± 0.833	5.557 ± 0.513	12.132 ± 1.001
UEA882	0.47	10.775 ± 0.690	5.865 ± 0.388	$10.406 \pm 0.56/$



Figure B1. Isotope data plotted as 230 Th/ 232 Th vs. 234 U/ 232 Th. The slope of the line gives the authigenic 230 Th/ 234 U composition of the carbonate (0.63).



Figure B2. Isotope data plotted as ${}^{234}U/{}^{232}$ Th vs. ${}^{238}U/{}^{232}$ Th. The slope of the line gives the authigenic ${}^{234}U/{}^{238}U$ composition of the carbonate (1.83).

Results

The isotope ratios 230 Th/ 234 U and 234 U/ 238 U are directly given by the slopes of the best-fit lines in the plotted coordinates chosen here. The isotope pair data for one particular sample, UEA882, generate a point which, on the 230 Th/ 232 Th versus 234 U/ 232 Th diagram, lies more than three standard deviations from the best-fit regression line,

Table B2. Age data derived from isochron plots. Six-point plots exclude sample 882 only. Fivepoint plots exclude UEA882 and UEA802. MSWD (mean square of weighted deviates) values indicate how closely the observed data scatter matches the scatter predicted from the errors and error correlations of the data points. P = probability of fit. Errors are 1 standard deviation. *Robust regression; ** model 1 regression (Ludwig 2001).

	230Th/234U	MSWD	Р	²³⁴ U/ ²³⁸ U	MSWD	Р	Age (ka)
Six points*	$0.65^{+0.37}_{-0.30}$		_	1.82 ± 0.17	0.25	0.86	103^{+164}_{-57}
Five points**	0.63 ± 0.11	0.51	0.68	1.82 ± 0.17	0.25	0.86	99^{+30}_{-24}

Table B3. Stable isotope data for Sefidabeh carbonates.

Sample no.	$\delta^{13}C$	$\delta^{18}O$	Material sampled
S7	-7.15	-5.70	Clotted micritic fenestral fabrics with Three stages of early diagenetic cements
S6	-7.03	-5.64	Clotted micritic fenestral fabrics with Some early diagenetic cementation
S5	-7.05	-5.74	Clotted micritic fabrics
S3	-7.20	-5.41	Clotted micritic fabric
Mean	-7.11	-5.62	

and on the ²³⁴U/²³²Th versus ²³⁸U/²³²Th diagram a point, which is unique in lying more than one standard deviation from the line. Either the more concentrated acid leach applied to this sample (see above) preferentially solubilized both uranium isotopes relative to thorium, or the detritus in this subsample may possess a different isotopic composition to the others. This sample has been omitted from the isochron diagrams. The same is probably true of the anomalous sample referred to in the main text, UEA802, to a lesser degree. Ages have been derived from both a five-data-point plot (Figs B1 and B2), excluding both 802 and 882, and a six-data-point plot, retaining 802. Table B2 summarizes the dating information drawn from the isochrons.

B3 Stable isotopes

Subsamples of 2–5 mg for stable isotope analysis were drilled from slabbed and polished hand specimens. Organic matter was removed by low temperature plasma ashing and the samples were then processed using normal laboratory procedures and measured on a VG Sira Series II mass spectrometer calibrated using the NBS 18 and NBS 19 standards. Isotopic data are reported in delta notation relative to the Vienna Pee Dee Belemnite (VPDB) international scale (Coplen 1994). Precision for the laboratory standard and duplicates at UEA was in both cases better than $\pm 2\sigma 0.06\%$ for δ^{13} C and $\pm 2\sigma 0.10\%$ for δ^{18} O. Measurements on four of the Sefidabeh samples are given in Table B3.

The mean δ^{18} O value for the calcite precipitate is -5.6% VPDB, with little variance between samples. Assuming equilibrium fractionation and temperatures of calcite formation in the range 20–30°C, these calcite δ^{18} O values correspond to water δ^{18} O values of between -4.7 and -2.6% VSMOW (Vienna Standard Mean Ocean Water), using the Hays & Grossman (1991) equation.

Given that there are multiple generations of cementation in these calcretes the isotopic data will be recording an average value of micrite and various microspars and sparry calcite cements. Although the latter are of small mass they cannot be ignored totally, and may affect the bulk isotopic composition a little (probably resulting in slightly more negative δ^{18} O value than in pure micrite).

Modern average δ^{18} O for rainfall at the latitude of central Iran is expected to be in the range -2 to -4% VSMOW (Yurtsever 1975), although in continental settings this will be modified toward lighter values by both continentality (i.e. prolonged moisture transport over land) and orographic (altitude) effects. Thus the weighted mean value at Tehran is -6.3% VSMOW and at Kabul is -7.1%VSMOW, both of which are relatively higher and further inland. By contrast, the weighted mean at Bahrain, in the Persian Gulf, is -0.9% VSMOW (all from Rozanski *et al.* 1993).

If the waters that precipitated the calcites had not evaporated much they might indicate equilibrium with meteoric waters with δ^{18} O values similar to today. However, the association of evaporite salts and calcite cementation point to at least seasonal aridity, suggesting that the waters that precipitated the calcites would have been evaporated somewhat. This being so, the isotopic composition of recharge would be more negative than -2.5% VSMOW (minimum) and probably more negative than -5.0% VSMOW. Air masses originating from the south or southwest of the study site would be maritime oceanic and too isotopically enriched to be the source of recharge came from the west or northwest and had significant continental/orographic effects that resulted in rainfall with isotopically light δ^{18} O.

However, there is also evidence from Oman that the Indian Ocean monsoon system moved further north in the past (during OIS 5a, 5e, 7a and 9 Burns *et al.* 1998, 2001). Large negative δ^{18} O values of recharge in the Sefidabeh region could therefore also be due to rainout effects caused by monsoon rainfall, providing an alternative explanation to that given above. Thus, while the precision on the age of the deposit is not critical for an estimate of fault growth rates, it is important for the palaeoclimatic interpretation. An age of 99–103 ka implies calcite formation in OIS 5c where the Oman record shows no evidence of wetter climate. However, the errors allow calcite formation in OIS 5e or 5a, monsoon influenced pluvials in Oman (Burns *et al.* 1998, 2001).

The δ^{18} O values taken alone are not diagnostic for choosing between the two climatic scenarios, that is, rainfall with strong continentality/orographic effects or rainfall with strong amount effects (monsoonal). The mean δ^{13} C value of -7.1% VPDB suggests a significant component of soil carbon incorporation in the calcite. The negative value also suggests that CO₂ degassing at the springs was not vigorous enough to have fractionated the carbon isotopes (*cf.* Ferguson *et al.* 1982). Calcrete δ^{13} C values of -7 to -8.6%VPDB in 5–19 ka Thar desert pedogenic calcretes have been taken to indicate wet climatic conditions (Singhvi *et al.* 1996).